

MM4 System's Poles and Feedback Characteristics



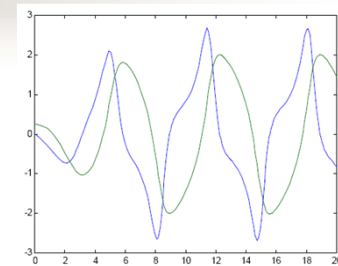
Readings:

- Section 3.3 (response & pole locations, p.118-126);
- Section 4.1 (basic properties of feedback, p.167-179);
- Extra readings (feedback characteristics)

What have we talked in **MM3**?

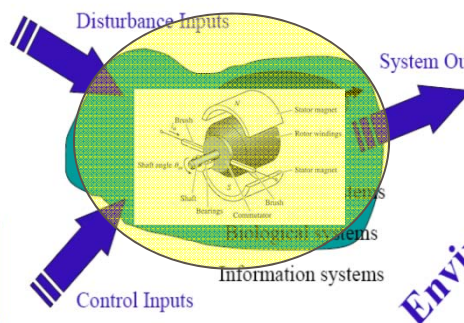
- The reponse analysis
- Performance specification
- Numerical simulation

MM3: Time Response Analysis (I)

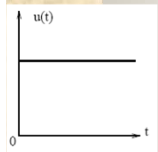


"help ode23" to find out all the other options.

$$d(t)=0$$



$$\theta_m = f(\theta_m(0), \dot{\theta}_m(0), v_a, T_e, T_f)$$



Typical input $u(t)$

Time response $y(t)$

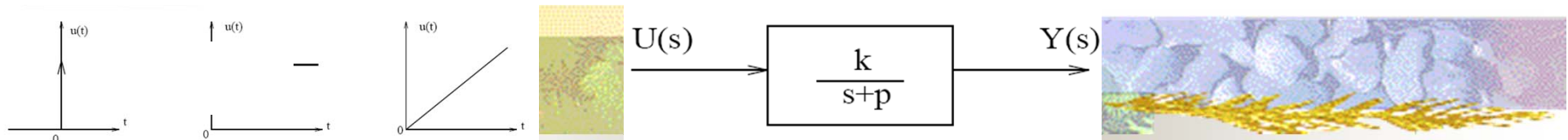
Laplace Trans

$$\theta_m(0) = \alpha, \quad \dot{\theta}_m(0) = \beta$$

$$Y(s) = G(s)U(s)$$

$$G(s) = \frac{\sum_{i=0}^m b_i s^i}{\sum_{i=0}^n a_i s^i}$$

Inv Laplace T.



MM3: Time Response Analysis (II)

- Typical inputs: impulse, step and ramp signals
- 1st, 2nd and high-order (LTI) systems

Test signal	$u(t)$	$U(s)$
Impulse	$\delta(t)$	1
Step	1	$1/s$
Ramp	t	$1/s^2$

$$G(s) = \frac{k}{s+p}, \quad \text{pole: } -p, \quad \text{time constant: } \frac{1}{p}$$

$$G(s) = \frac{c}{\tau s + 1}, \quad \text{pole: } -\frac{1}{\tau}, \quad \text{time constant: } \tau$$

time domain :

$$g(t) = ke^{-pt} \quad \text{or} \quad g(t) = \frac{c}{\tau} e^{-\frac{1}{\tau}t}$$

$$G(s) = \frac{\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}$$

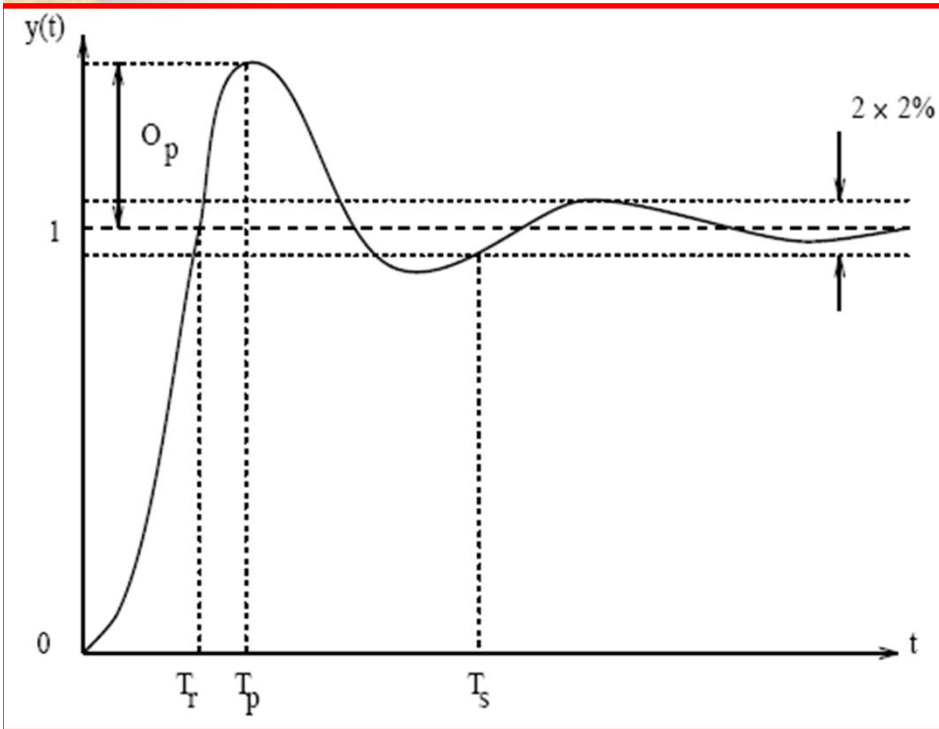
- ξ – *damping ratio*, a dimensionless factor
- ω_n – *natural frequency* with unit rad/s

Time response = excitation response + initial condition response (free response)

$$\phi = \tan^{-1} \frac{\sqrt{1-\xi^2}}{\xi}, \quad \omega_d = \omega \sqrt{1-\xi^2}$$

$$G(s) = \frac{\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}$$

MM3: Performance Specification



$$t_r \cong \frac{1.8}{\omega_n}$$

$$t_s \cong \frac{4.6}{\zeta\omega_n} \cong \frac{4.6}{\sigma}$$

$$M_p \cong \begin{cases} 5\%, & \zeta = 0.7 \\ 16\%, & \zeta = 0.5 \\ 35\%, & \zeta = 0.3 \end{cases}$$

$$t_p \cong \frac{\pi}{\omega_d}, \quad \omega_d = \omega_n \sqrt{1-\zeta^2}$$

$$\text{Rise time } T_r = \frac{\pi - \phi}{\omega_d}$$

$$\text{Peak time } T_p = \frac{\pi}{\omega_d}$$

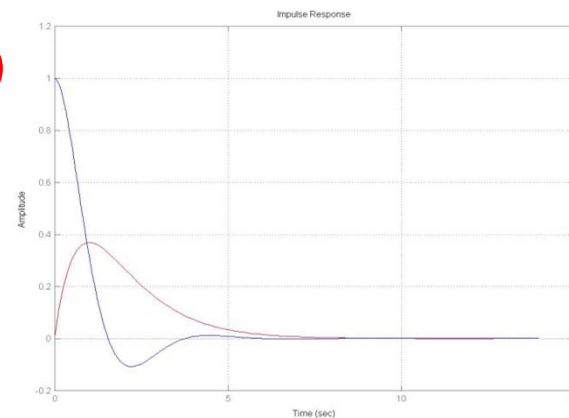
$$\text{Settling time } T_s \approx \frac{4}{\xi\omega_n}$$

$$\text{Overshoot } O_p = e^{-\frac{\xi\pi}{\sqrt{1-\xi^2}}}$$

Steady-state error e_{SS} : difference between input & output as $t \rightarrow \infty$

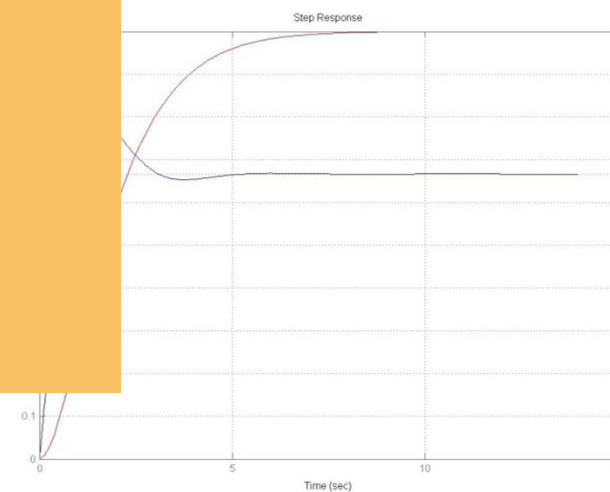
MM3: Numerical Simulation

- Impulse response: **impulse(sys)**
- Step response: **step(sys)**
- **ltiview(sys)**
- **Subplot(m,n,1)**



EXAMPLE:

```
sys1:          Sys2:  
num1=[1];      num2=[1 2];  
den1=[1 2 1];  den2=[1 2 3];  
impulse(tf(num1,den1),'r',tf(num2,den2),'b')  
step(tf(num1,den1),'r',tf(num2,den2),'b')
```



Goals for this lecture (MM4)

- System poles vs. time responses
 - Poles and zeros
 - Time responses vs. Pole locations
- Feedback characteristics
 - Characteristics
 - A simple feedback design
- Block diagram decomposition (simulink)

System Poles

- First-order system

$$G(s) = \frac{k}{s+p}, \quad \text{pole: } -p, \quad G(s) = \frac{c}{\tau s+1}, \quad \text{pole: } -\frac{1}{\tau}$$

- Second-order system

$$G(s) = \frac{\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2},$$

$$\text{poles: } p_{1,2} = -\xi\omega_n \pm \omega_n \sqrt{\xi^2 - 1}$$

$$\text{real (different) poles: } p_{1,2} = -\xi\omega_n \pm \omega_n \sqrt{\xi^2 - 1}, \quad \text{if } \xi > 1$$

$$\text{real (identical) poles: } p_{1,2} = -\xi\omega_n, \quad \text{if } \xi = 1$$

$$\text{complex poles: } p_{1,2} = -\xi\omega_n \pm j\omega_n \sqrt{1 - \xi^2}, \quad \text{if } 0 < \xi < 1$$

$$\text{complex poles: } p_{1,2} = \pm j\omega_n, \quad \text{if } \xi = 0$$

- High-order system

$$G(s) = \frac{\sum_{i=0}^m b_i s^i}{\sum_{i=0}^n a_i s^i} = \frac{(s+z_1)(s+z_2)\cdots(s+z_m)}{(s+p_1)(s+p_2)\cdots(s+p_n)}$$

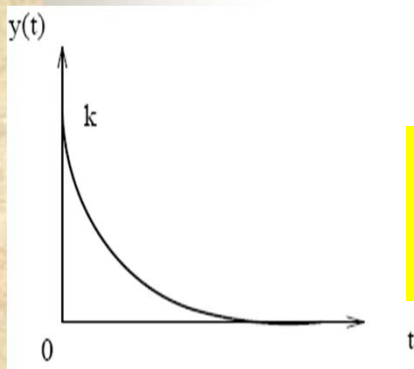
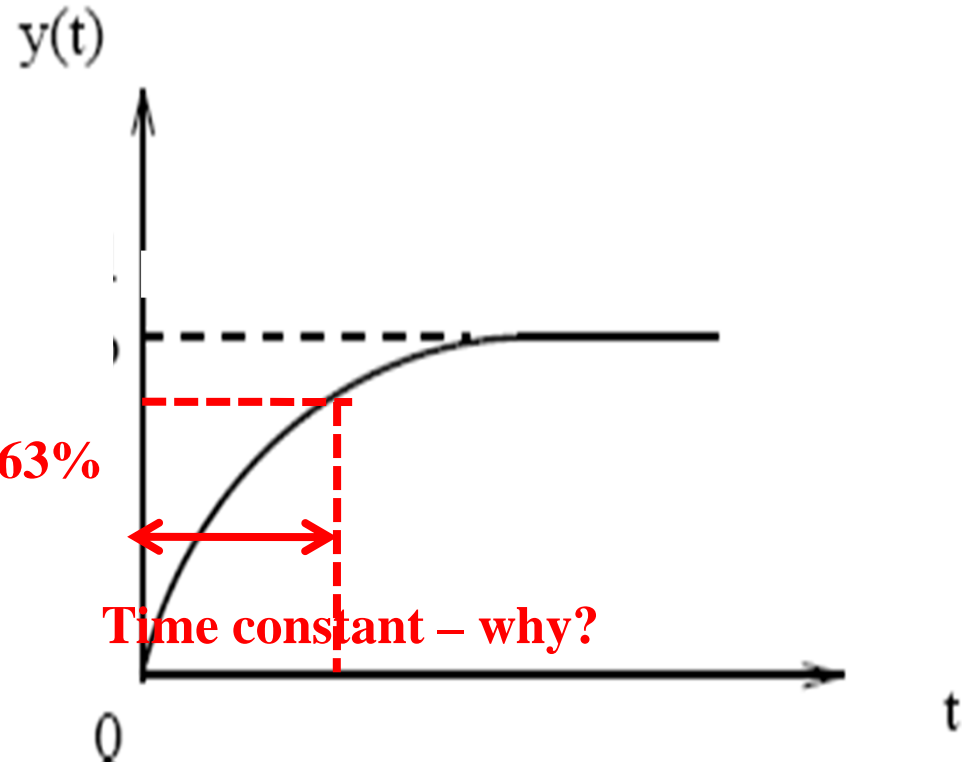
Pole vs Time Response: **First-order System (I)**

$$G(s) = \frac{1}{\tau s + 1}, \quad \text{assume } \tau > 0$$

pole: $-\frac{1}{\tau}$, time constant: τ ,

Impulseresponse: $y(t) = L\left(\frac{1}{\tau s + 1}\right) = e^{-\frac{1}{\tau}t}$

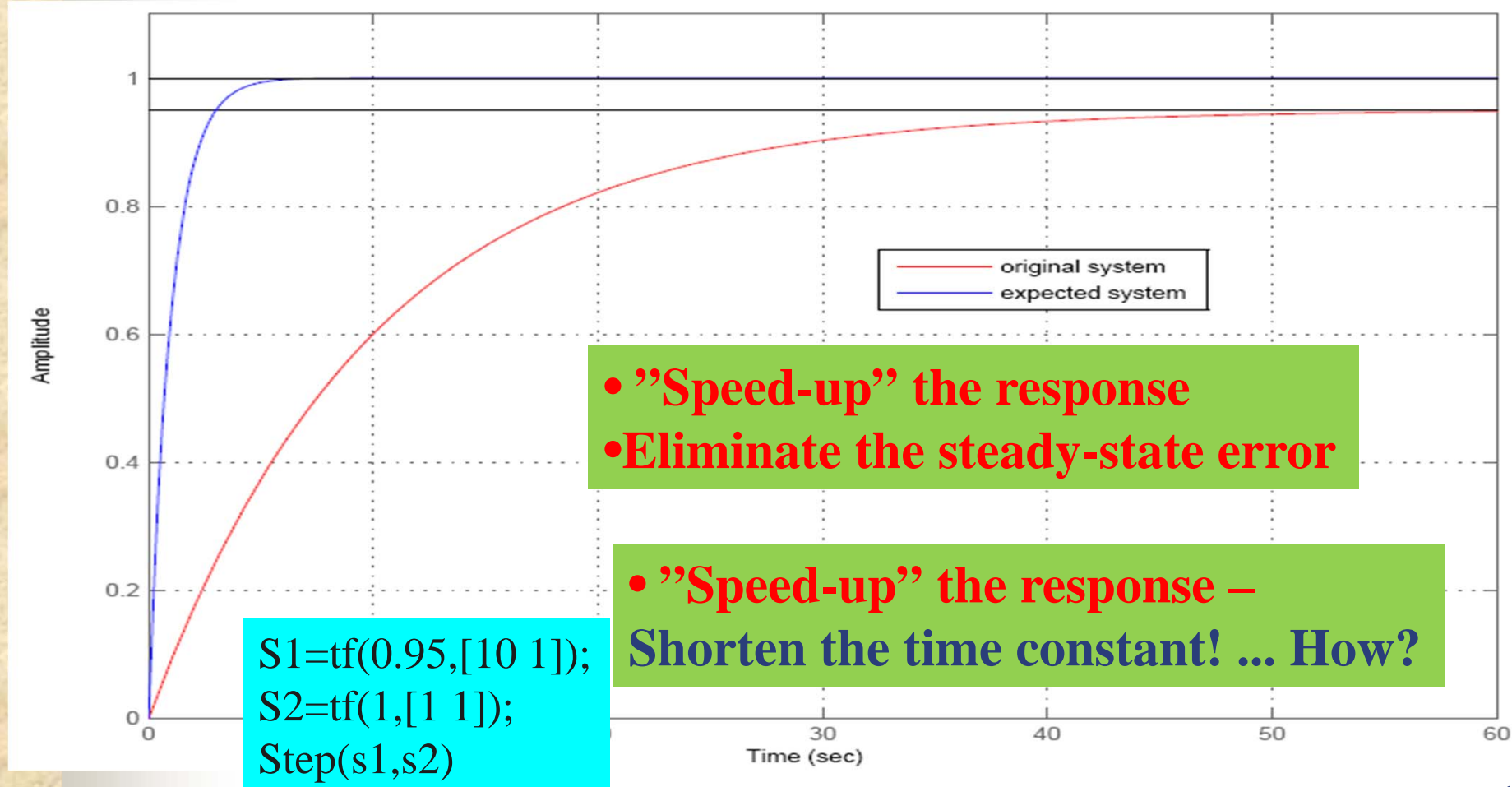
Stepresponse: $y(t) = L\left(\frac{1}{s(\tau s + 1)}\right) = 1 - e^{-\frac{1}{\tau}t}$



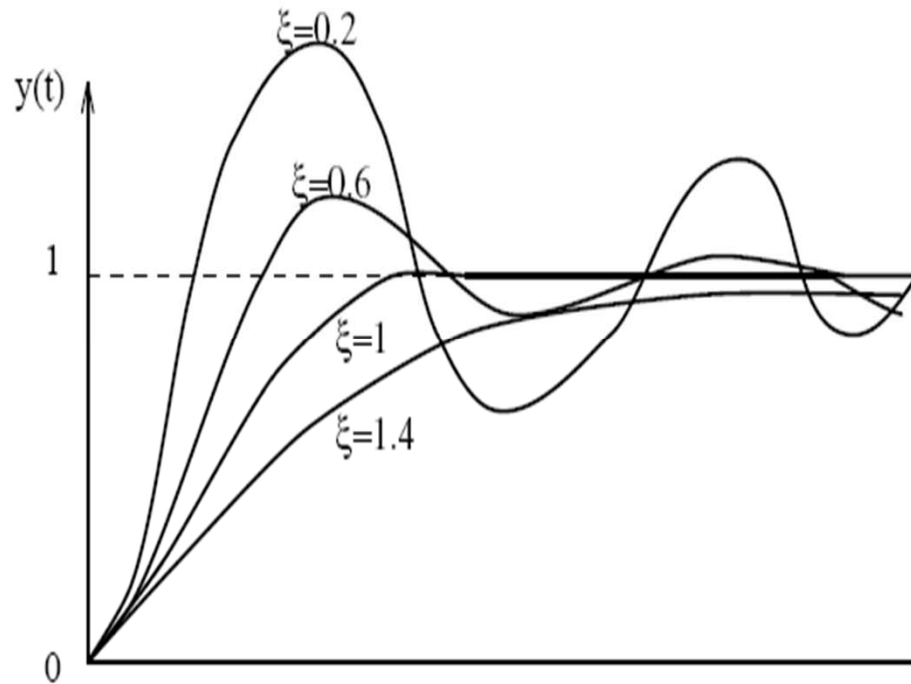
Time response is determined by the time constant
System pole is the negative of inverse time constant

Pole vs Time Response: **First-order System (II)**

- An design problem – how to use this knowledge



Time Response: 2nd-order System (I)



$$G(s) = \frac{\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}$$

- ξ – *damping ratio*, a dimensionless factor
- ω_n – *natural frequency* with unit rad/s

Summary: The response

- converges to 1 due to $e^{-\xi\omega_n t}$;
- oscillates at frequency ω_d if $0 < \xi < 1$;
- has no oscillation if $\xi \geq 1$;
- possesses larger amplitude of the initial response period for smaller ξ ;
- equals $y(t) = 1 - \cos\omega_n t$ for the extreme case: $\xi = 0$

$\xi = 0$	Undamped
$\xi < 1$	Underdamped
$\xi = 1$	Critically damped
$\xi > 1$	Overdamped

Time Response: 2nd-order System (II)

$$G(s) = \frac{\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}, \quad \text{assume } \omega_n > 0, \quad \xi \geq 0$$

poles: $p_{1,2} = -\xi\omega_n \pm \omega_n\sqrt{\xi^2 - 1}$

real(different) poles: $p_{1,2} = -\xi\omega_n \pm \omega_n\sqrt{\xi^2 - 1}$, if $\xi > 1$

real(identical) poles: $p_{1,2} = -\xi\omega_n$, if $\xi = 1$

complex poles: $p_{1,2} = -\xi\omega_n \pm j\omega_n\sqrt{1 - \xi^2}$, if $0 < \xi < 1$

complex poles: $p_{1,2} = \pm j\omega_n$, if $\xi = 0$

$$G(s) = \frac{\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}$$

ξ – *damping ratio*, a dimensionless factor

ω_n – *natural frequency* with unit rad/s

Summary: The response

converges to 1 due to $e^{-\xi\omega_n t}$;

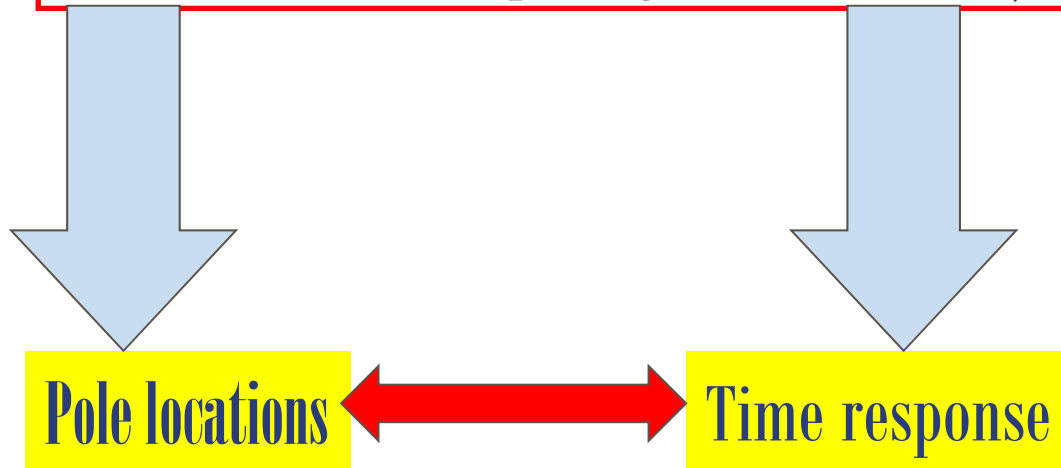
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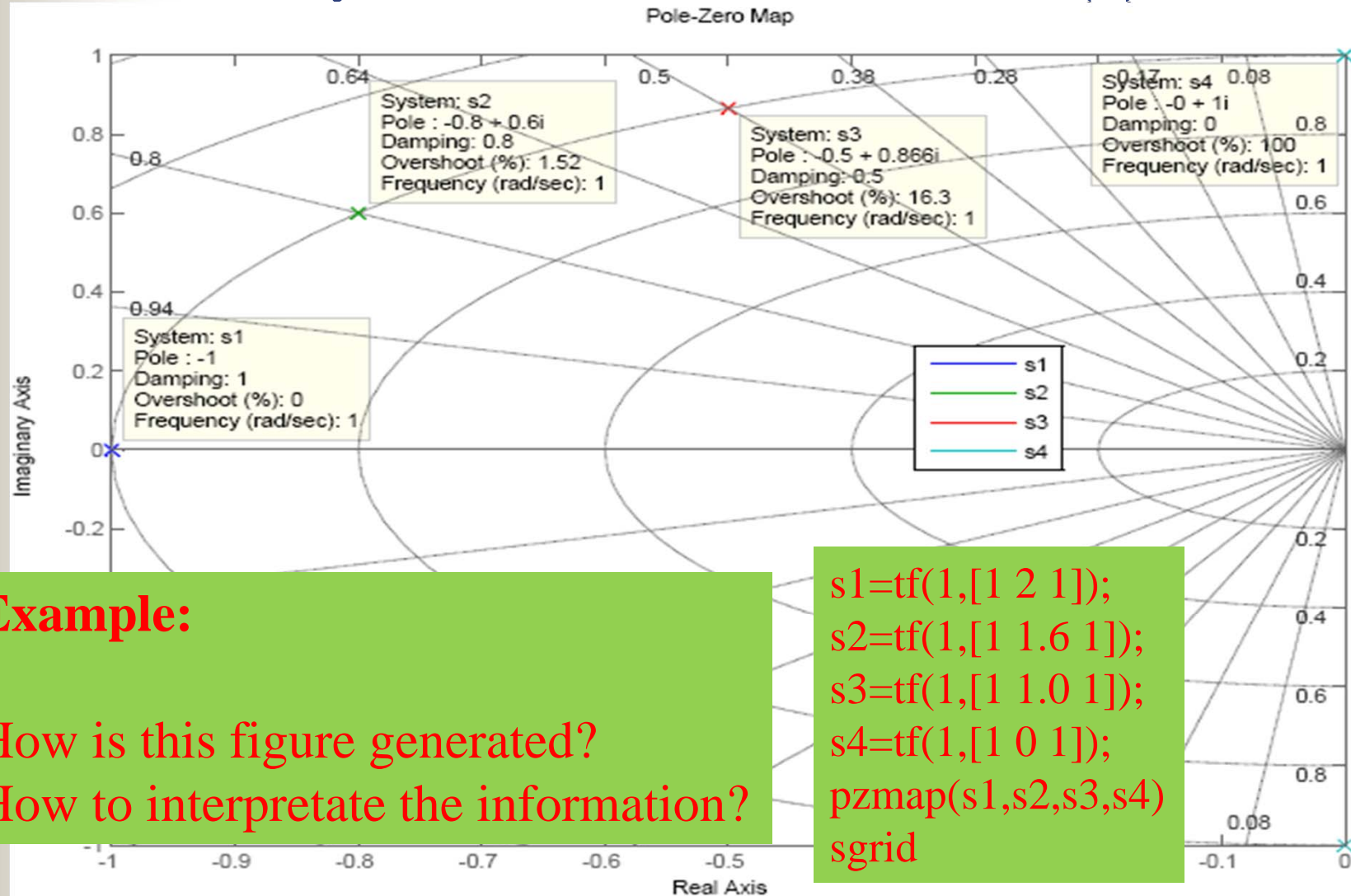
2nd-order System: **Poles vs Performance**

$$G(s) = \frac{\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}.$$

- ξ – *damping ratio*, a dimensionless factor
- ω_n – *natural frequency* with unit rad/s



2nd-order System – Pole Locations (I)



Example:

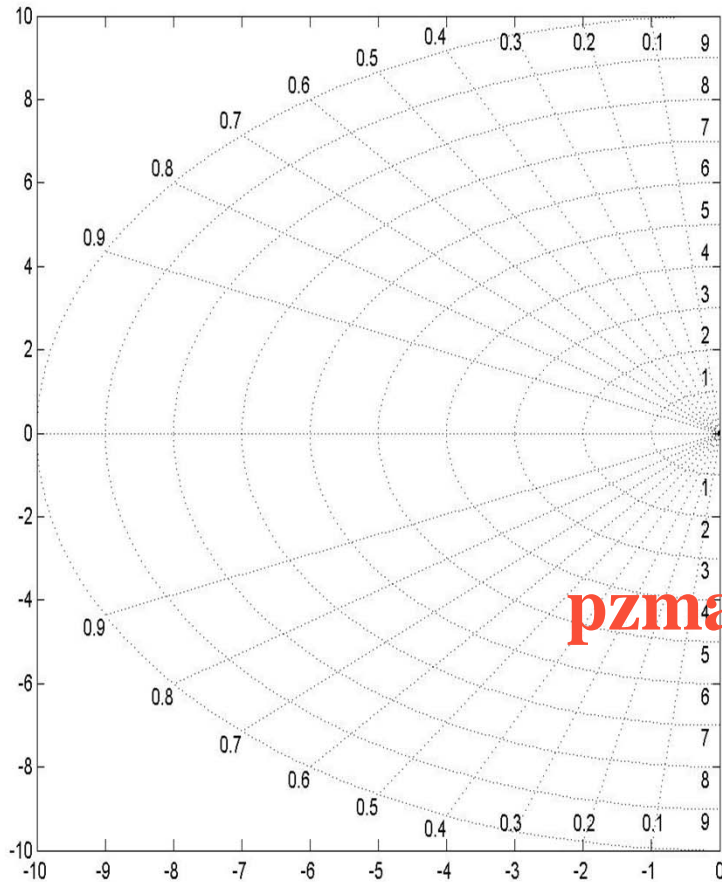
How is this figure generated?

How to interpretate the information?

```

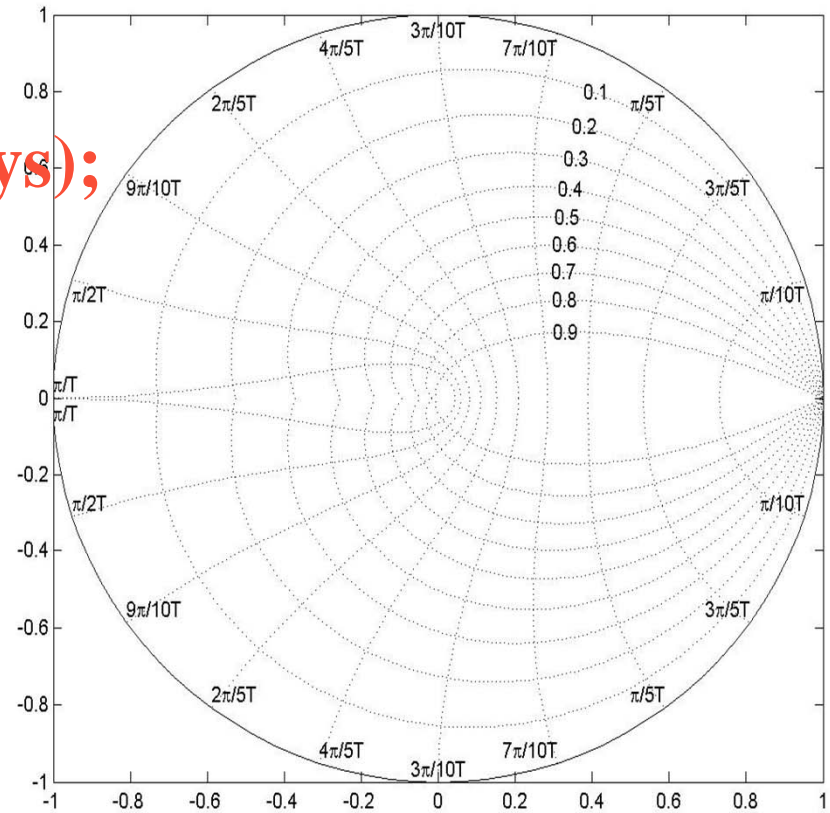
s1=tf(1,[1 2 1]);
s2=tf(1,[1 1.6 1]);
s3=tf(1,[1 1.0 1]);
s4=tf(1,[1 0 1]);
pzmap(s1,s2,s3,s4)
sgrid
    
```

SGRID generates a grid over an existing continuous s-plane root locus or pole-zero map. Lines of constant damping ratio (zeta) and natural frequency (ω_n) are drawn.



pzmap(Sys);

ZGRID generates a grid over an existing discrete z-plane root locus or pole-zero map. Lines of constant damping factor (zeta) and natural frequency (ω_n) are drawn in within the unit Z-plane circle.



2nd-order System – Pole Locations (II)

$$G(s) = \frac{\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}, \quad \text{assume } \omega_n > 0, \quad \xi \geq 0$$

poles: $p_{1,2} = -\xi\omega_n \pm \omega_n\sqrt{\xi^2 - 1}$

real(different) poles: $p_{1,2} = -\xi\omega_n \pm \omega_n\sqrt{\xi^2 - 1}$, if $\xi > 1$

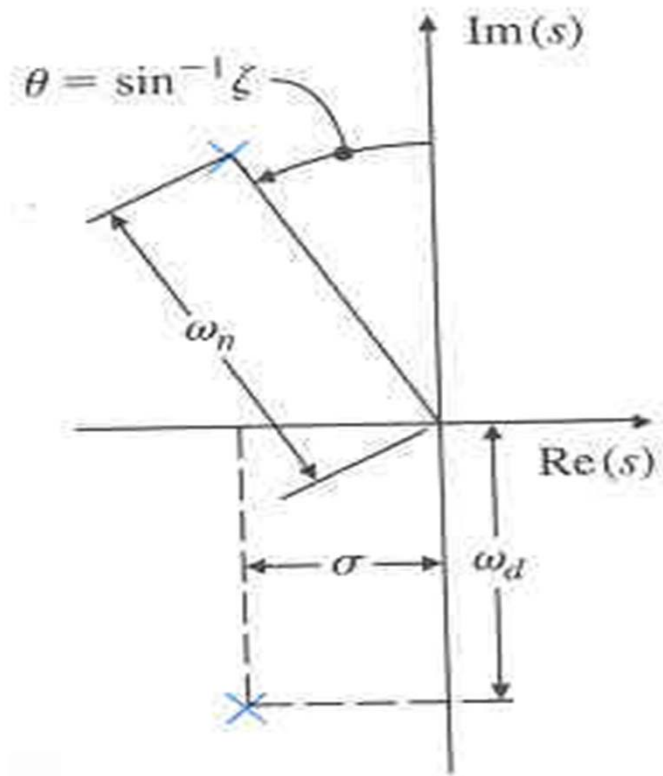
real(identical) poles: $p_{1,2} = -\xi\omega_n$, if $\xi = 1$

complex poles: $p_{1,2} = -\xi\omega_n \pm j\omega_n\sqrt{1 - \xi^2}$, if $0 < \xi < 1$

complex poles: $p_{1,2} = \pm j\omega_n$, if $\xi = 0$

FIGURE 3.11

s -plane plot for a pair of complex poles



2nd-order System – Pole Locations (III)

Exercise:

- (1) Figure out the damping ratio and natural frequency of the following systems
- (2) Sketch all pole locations in the s-plane according to the information you get from (1)
- (3) Sketch and compare the step responses of all systems, and explain the results

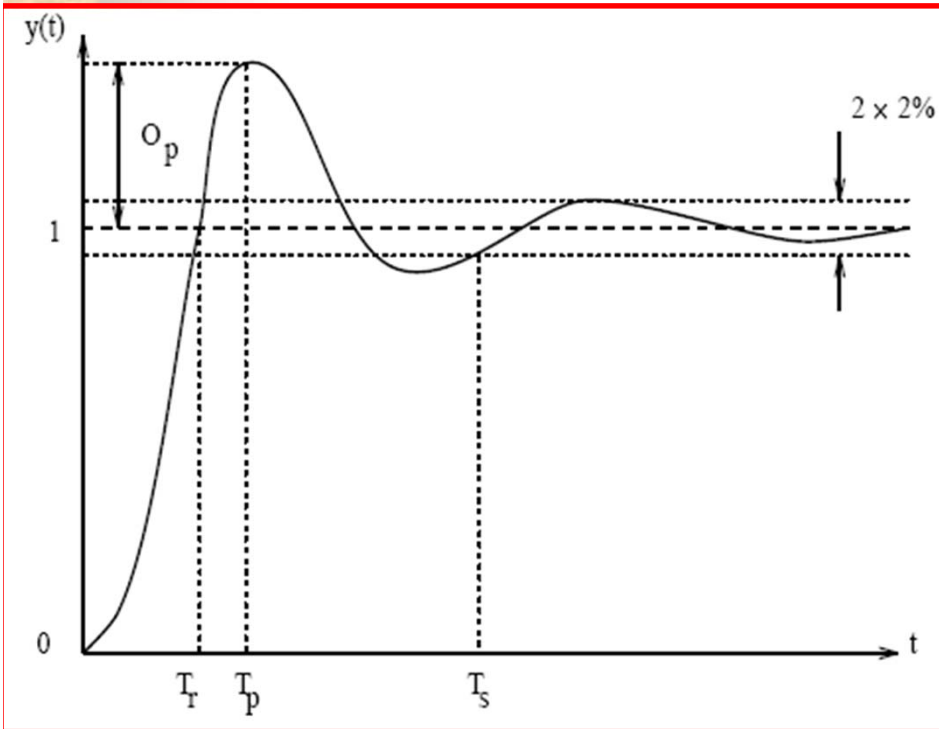
```
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s3=tf(1,[1 1.0 1]);  
s4=tf(1,[1 0 1]);  
pzmap(s1,s2,s3,s4)  
sgrid
```



$$\phi = \tan^{-1} \frac{\sqrt{1-\xi^2}}{\xi}, \quad \omega_d = \omega \sqrt{1-\xi^2}$$

$$G(s) = \frac{\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}$$

MM3: Performance Specification



$$t_r \cong \frac{1.8}{\omega_n}$$

$$t_s \cong \frac{4.6}{\zeta\omega_n} \cong \frac{4.6}{\sigma}$$

$$M_p \cong \begin{cases} 5\%, & \zeta = 0.7 \\ 16\%, & \zeta = 0.5 \\ 35\%, & \zeta = 0.3 \end{cases}$$

$$t_p \cong \frac{\pi}{\omega_d}, \quad \omega_d = \omega_n \sqrt{1-\zeta^2}$$

$$\text{Rise time } T_r = \frac{\pi - \phi}{\omega_d}$$

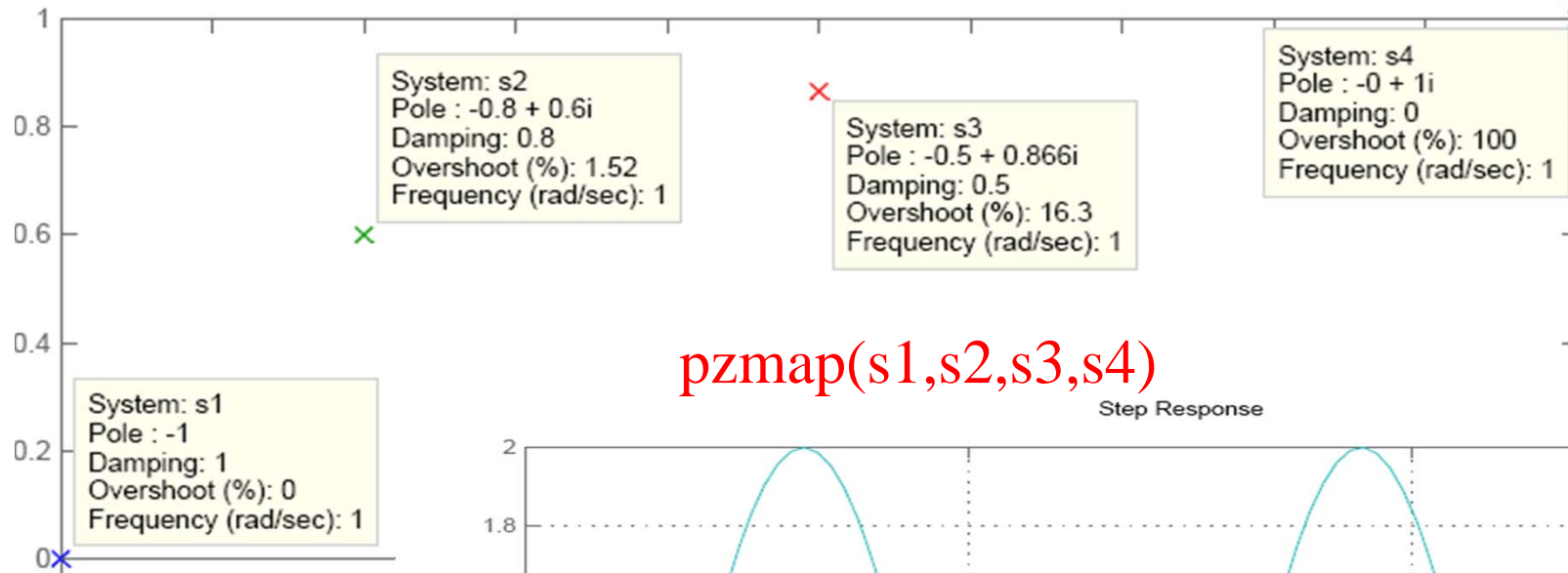
$$\text{Peak time } T_p = \frac{\pi}{\omega_d}$$

$$\text{Settling time } T_s \approx \frac{4}{\xi\omega_n}$$

$$\text{Overshoot } O_p = e^{-\frac{\xi\pi}{\sqrt{1-\xi^2}}}$$

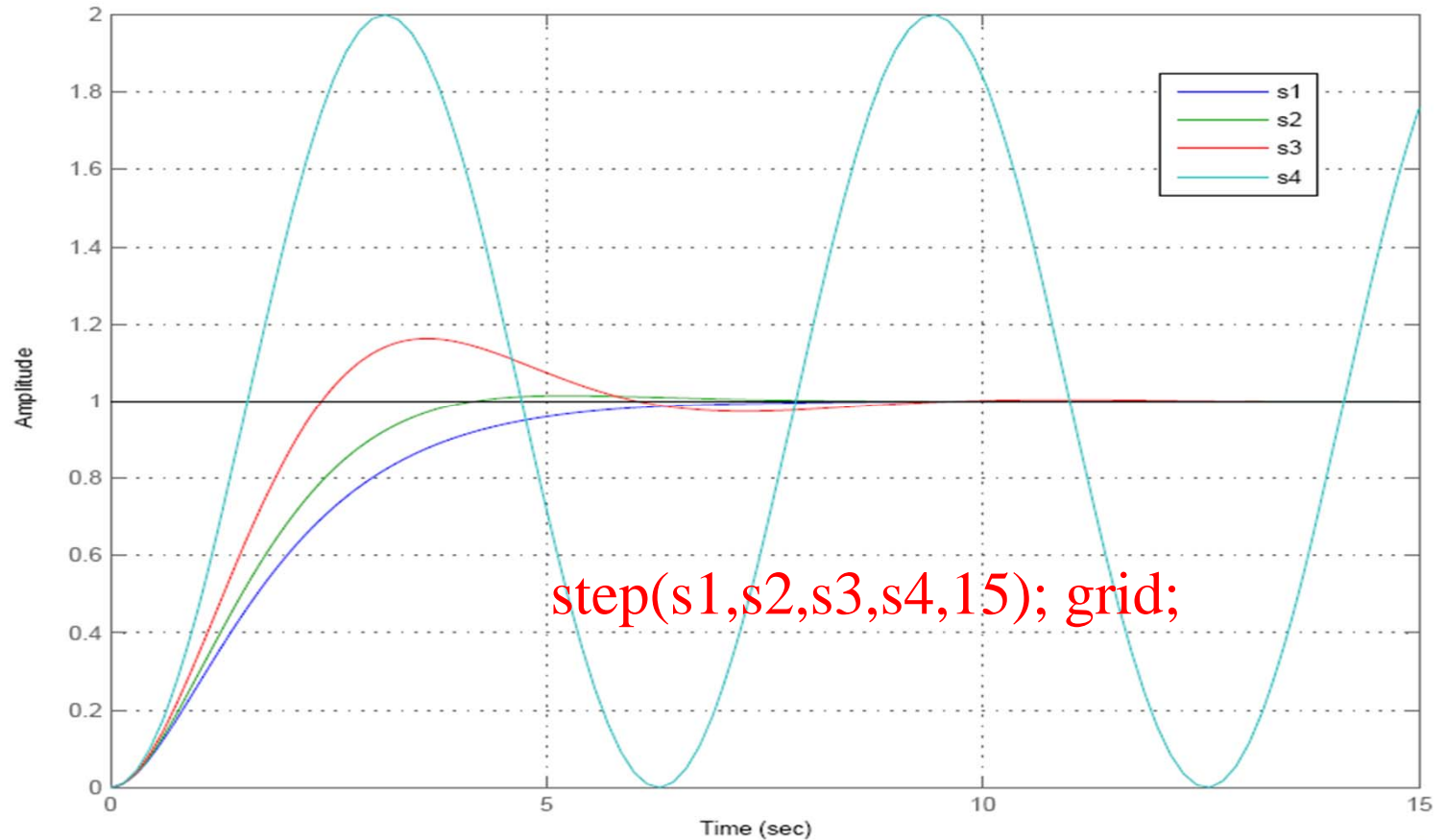
Steady-state error e_{ss} : difference between input & output as $t \rightarrow \infty$

Pole-Zero Map



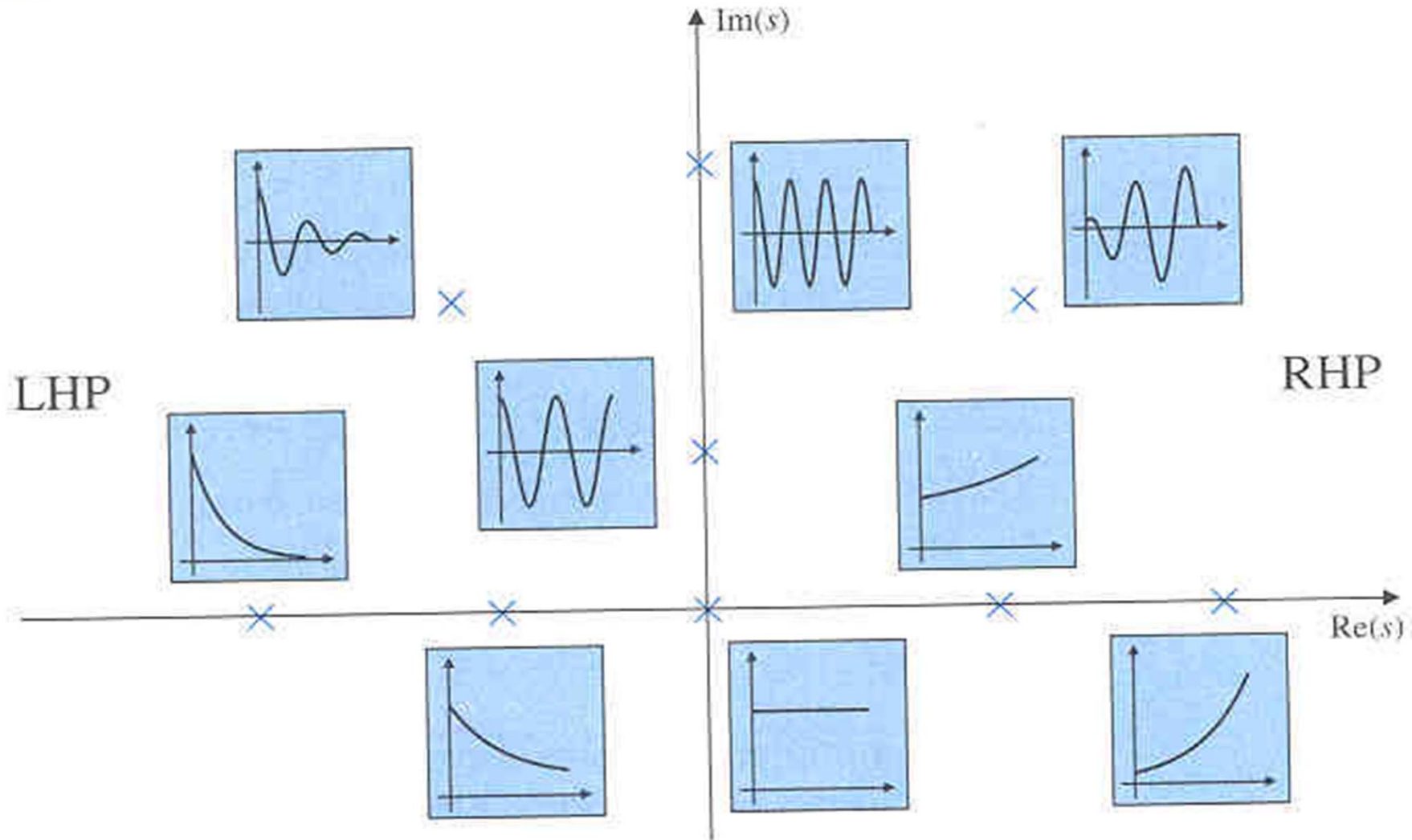
`pzmap(s1,s2,s3,s4)`

Step Response



`step(s1,s2,s3,s4,15); grid;`

Summary of Pole vs Performance (I)



Summary of Pole vs Performance (II)

$$G(s) = \frac{\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}$$

$$\phi = \tan^{-1} \frac{\sqrt{1-\xi^2}}{\xi}, \quad \omega_d = \omega \sqrt{1-\xi^2}$$

- ξ – *damping ratio*, a dimensionless factor
- ω_n – *natural frequency* with unit rad/s

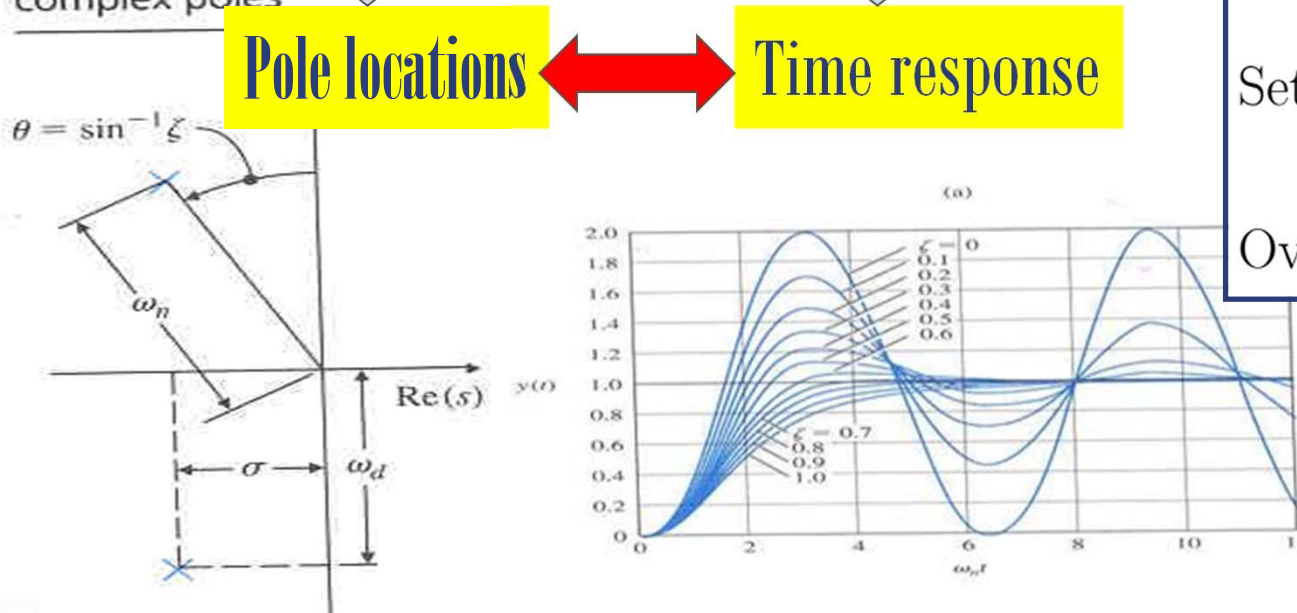
$$\text{Rise time } T_r = \frac{\pi - \phi}{\omega_d}$$

$$\text{Peak time } T_p = \frac{\pi}{\omega_d}$$

$$\text{Settling time } T_s \approx \frac{4}{\xi\omega_n}$$

$$\text{Overshoot } O_p = e^{-\frac{\xi\pi}{\sqrt{1-\xi^2}}}$$

FIGURE 3.11 s -plane plot for complex poles



Pole locations

Time response

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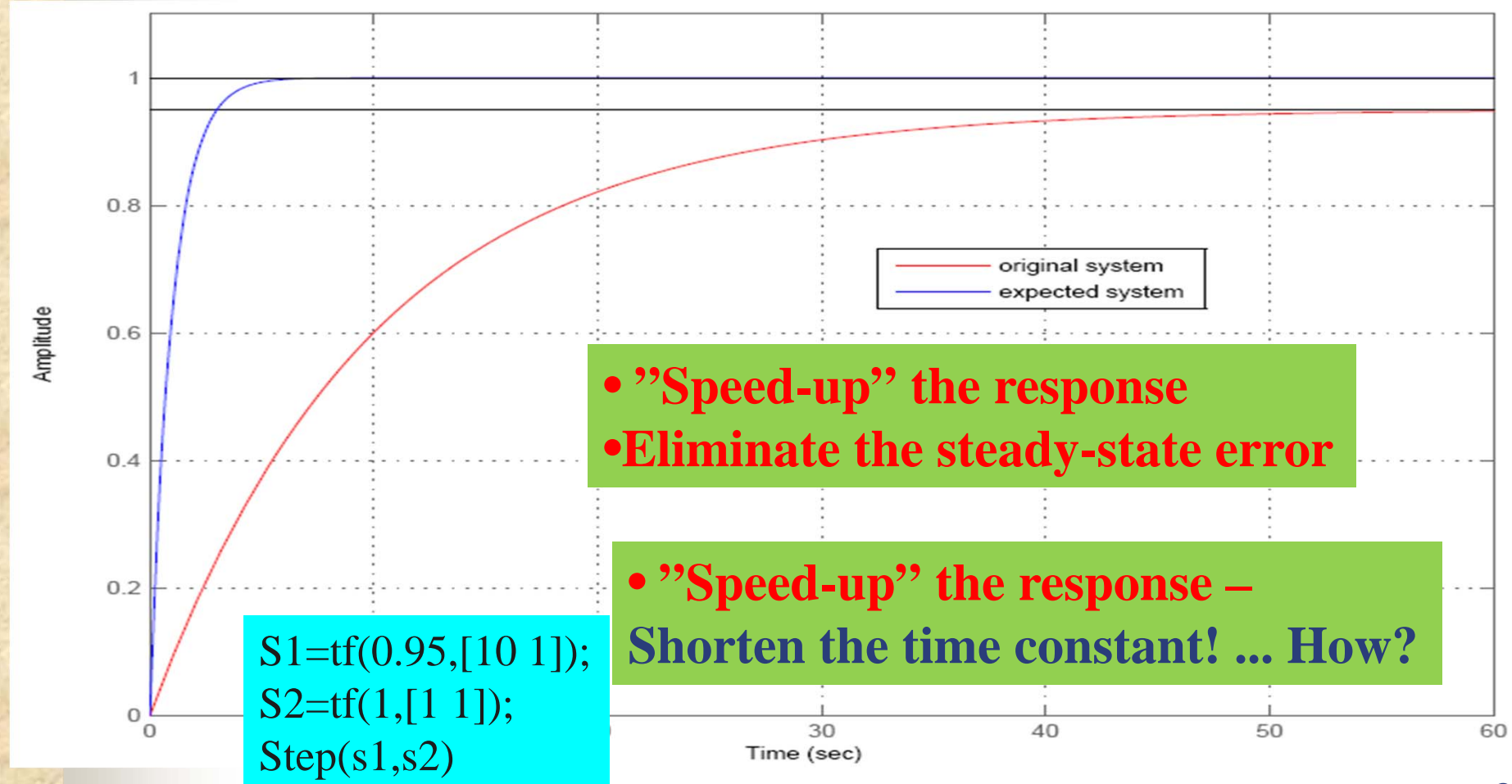
See chapter 2 of Goodwin et al



Material can be downloaded from
course webpage

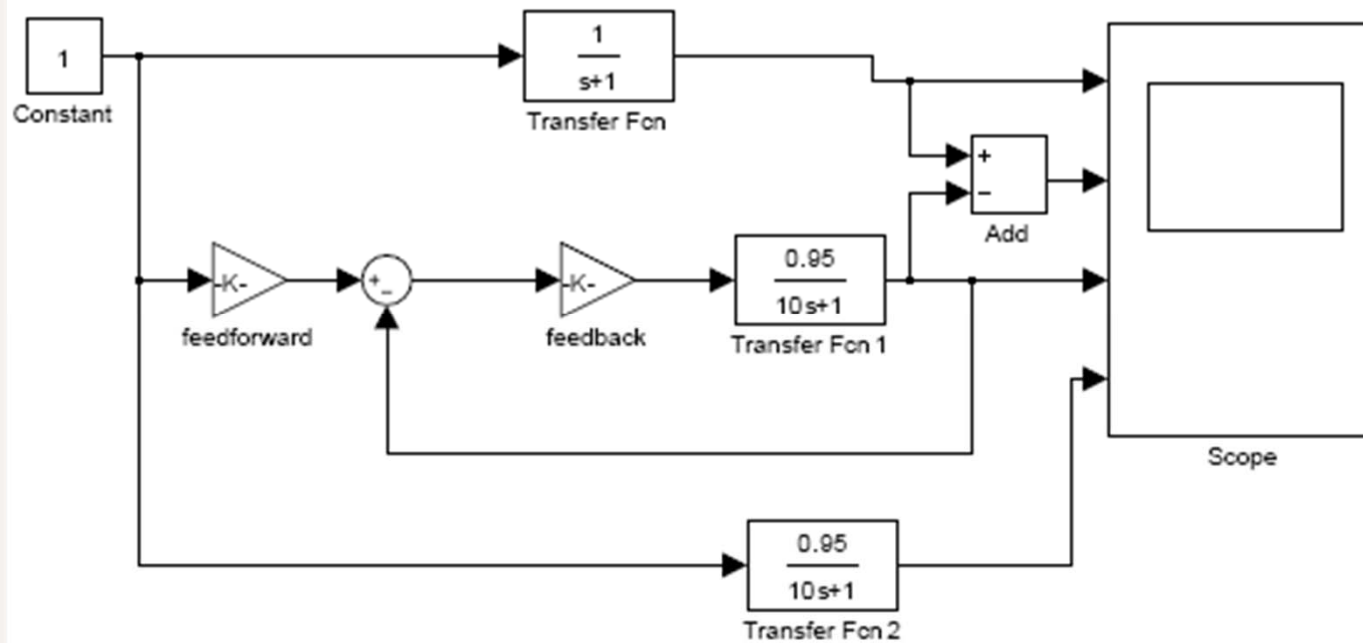
Revisit of example : First-order System (I)

- An design problem – how to use this knowledge



Revisit of example : First-order System (II)

- A design solution



[Download feedbackexample.mdl](#)



Summary of Feedback Characteristics

- System errors can be made less sensitive to disturbance with feedback than they are in open-loop systems
- In feedback control, the error in the controlled quantity is less sensitive to variations in the system gain/parameters
- Design tradeoff between gain and disturbance

Goals for this lecture (MM4)

- System poles vs. time responses
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See blackboard